# **Lattice-Boltzmann Models of Ion Thruster Cathode 3D MHD Flows**

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**Ion thrusters are the most efficient EP devices at converting input power to thrust and are used both as primary propulsion and for station-keeping on commercial and scientific spacecraft.**

*•* Department of Aerospace Engineering• **Key issues include grid erosion and thrust density limitations from space-charge effects.**  $\overline{\phantom{a}}$ 

# Modern Ion Thrusters

**Solar Electric Propulsion — NASA's Evolutionary Xenon Thruster (NEXT) [5-10 yr. deployment time]** **Nuclear Electric Propulsion — NASA's Nuclear Space Initiative [10-15 yr. deployment time]**



# Typical Ion Engine Parameters

 Near DCA & grid, typical ion thruster & plasma parameters are:

*nXe+*~ 1013-1010 cm-3 , *n<sup>e</sup>* ~ 1013-1010 cm-3 >> *nXe* >> *nXe++* …

- $V_+$  ~ 1075 V at screen grid
- $V 150$  V at accelerator grid
- Grid separation  $\sim$  1 mm
- Screen grid opening diameter  $\sim$  2 mm
- Accelerator grid opening diameter  $\sim$  1 mm
- $\blacksquare$  DCA  $V_{dc}$  = 25V difference from anode
- $\blacksquare$  B = 100G



## Assumptions of Applicability of LB

- Note local *Kn*: Crawford (2002)
- *Kn*  $\sim$  O(0.1) around optics & DCA
- Maxwellian radial *f(***v**)





ion speed (km/s) Ion veloc. distrib. Laser-induced Fluorescence Velocimetry of Xe II in the 30-cm NSTAR-type Ion Engine Plume, Smith and Gallimore (AIAA-2004-3963)



## **MHD Equations**

 $\overline{\phantom{a}}$ 

 $\overline{a}$  $\overline{a}$  $\overline{a}$  $\overline{a}$  $\overline{a}$  $\overline{a}$  $\overline{\phantom{a}}$ 

 $\lfloor$ 

 $\rho$ **v** 

 $BB -$ 

 $BB -$ 

1

 $\left( \mathbf{B} \mathbf{B} - \frac{1}{2} B^2 \mathbf{I} \right)$ 

 $\left( \mathbf{B}\mathbf{B}-\frac{1}{2}B^2\mathbf{I} \right)$ 

1

 $\left( \mathbf{B} \mathbf{B} - \frac{1}{2} B^2 \mathbf{I} \right)$ 

 $\left( \mathbf{B}\mathbf{B}-\frac{1}{2}B^2\mathbf{I} \right)$ 

2

2

/  $\overline{a}$   $\overline{\phantom{a}}$ 

 $\overline{\phantom{a}}$  $\overline{\phantom{a}}$  $\overline{\phantom{a}}$  $\overline{\phantom{a}}$  $\overline{\phantom{a}}$  $\overline{\phantom{a}}$  $\overline{\phantom{a}}$ 

 $= \nabla \bullet$ 

0

 $\overline{\phantom{a}}$ 

 $\overline{\phantom{a}}$  $\overline{\phantom{a}}$  $\overline{\phantom{a}}$  $\overline{\phantom{a}}$ 

 $\overline{\phantom{a}}$ 

 $\vert$ 

 $\overline{\phantom{a}}$  $\overline{a}$  $\overline{\phantom{a}}$  $\overline{\phantom{a}}$ 

 $\lfloor$ 

 $\tau_{_{vis}}$ 

**E***resist*

**q**

/ 0i**v**

 $\overline{\phantom{a}}$ 

1

 $\mu$ 

1

 $\mu$ 

 $\setminus$ 

 $\setminus$ 

 $vB - Bv$ 

 $\rho$ vv +  $p$ **I**  $-$ 

 $(E + p)\mathbf{v} -$ 

MHD eqs. comprise conservation of

 $\overline{\phantom{a}}$ 

 $\overline{\phantom{a}}$  $\overline{a}$  $\overline{\phantom{a}}$  $\overline{\phantom{a}}$   $\rho$ 

 $\overline{\phantom{a}}$ 

 $\overline{\phantom{a}}$  $\overline{\phantom{a}}$  $\overline{\phantom{a}}$  $\overline{\phantom{a}}$ 

 $+ \nabla \bullet$ 

 $\rho$ <mark>v</mark>

**B**

*E*

 $\overline{\phantom{a}}$ 

 $\lfloor$ 

 $\partial$ 

 $\partial t$ 

- mass,
- momentum,
- magnetic flux
- energy
- where

$$
-\nabla \bullet \mathbf{E}_{resist} = \nabla \times \left(\frac{1}{\sigma} \mathbf{j} + \frac{1}{en_e} \mathbf{j} \times \mathbf{B}\right) = \left[\eta_0 \vec{j}\right] - \left[\vec{\vec{\eta}} \bullet \vec{j}\right] + \left[\vec{\vec{\eta}} \bullet \vec{j}\right]^T
$$



• Department of Aerospace Engineering• © Dr. Jacques C. Richard

Sankaran (2001)

### LBM Basics

**The molecular velocity distribution function**  $f = f(x_i, c_i, t) = f(x, c, t)$  has a <u>rate of change</u>, w.r.t. position & time,

$$
\frac{\partial}{\partial t} \Big[ nf(c_i) \Big] + c_j \frac{\partial}{\partial x_j} \Big[ nf(c_i) \Big] = \left\{ \frac{\partial}{\partial t} \Big[ nf(c_i) \Big] \right\}_{collision}
$$
\n
$$
\left\{ \frac{\partial}{\partial t} \Big[ nf(c_i) \Big] \right\}_{collision} = \int_{-\infty}^{\infty} \int_{0}^{2\pi} \int_{0}^{2} n^2 d^2 \Big[ f(c'_i) f(z'_i) - f(c_i) f(z_i) \Big] g \sin \psi \cos \psi d\psi d\epsilon dV_x
$$

**- Macroscopic variables of interest** 

$$
\rho = \int_{-\infty}^{\infty} m f dV_c \qquad \rho \mathbf{u} = \int_{-\infty}^{\infty} m c f dV_c \qquad e_{tr} = \int_{-\infty}^{\infty} \frac{1}{2} m (\mathbf{c} - \overline{\mathbf{c}})^2 f dV_c
$$



#### The "1<sup>st</sup> Order" Boltzmann Equation

- So Boltzmann equation becomes, to 1<sup>st</sup> order:  $\partial f$  $\partial t$  $+ \mathbf{c} \cdot \nabla f = -$ 1  $\frac{1}{\lambda} (f - f^{(eq)}) =$ *df dt*
- On the characteristic line  $\mathbf{c} = d\mathbf{x}/dt$ , where  $\lambda = 1 / v_r$
- Integrating over a small time step  $\delta_t$ , assuming  $f^{(eq)}$  is smooth enough locally, and expanding in a Taylor series while neglecting terms of  $O(\delta_t^2)$  and also defining  $\tau = \lambda/\delta_t$ :

$$
f(\mathbf{x} + \mathbf{c}\delta_t, \mathbf{c}, t + \delta_t) - f(\mathbf{x}, \mathbf{c}, t) = -\frac{1}{\tau} \Big[ f(\mathbf{x}, \mathbf{c}, t) - f^{(eq)}(\mathbf{x}, \mathbf{c}, t) \Big]
$$



## 2D Square Lattice-Boltzmann Model 9-bit

- Cartesian coord, moment integral of  $I_m =$ *m*  $\int_{\pi}^{m} \sum_j \omega_i \omega_j \psi(c_{i,j})^2_1$  $c_{i,j} \bullet \mathbf{u}$ *kT* +  $(c_{i,j} \bullet \mathbf{u})^2$  $\frac{1}{2(kT)^2}$  –  $\mathbf{u}^2$ 2*kT*  $\mathfrak{f}$  $\left\{ \right.$ '  $\overline{\mathsf{I}}$ '  $\mathsf{I}$ \* |
|
|  $\left[\begin{array}{cc} kT & 2(kT)^2 & 2kT \\ kT & 2(kT)^2 & 2kT \end{array}\right]$ 3  $\sum$  $\psi_{mn}(\mathbf{c}) = c_x^m c_y^n$
- Select possible molecular velocities on 2D square lattice to go in as many directions of such square
- The chosen velocities have a certain symmetry to account for molecules moving in any and all directions independent of directions (isotropy)  $\epsilon$  2 4  $\epsilon$ 2
- For square this means sides & corners
- This means 9 possible velocities
- To go w/at least 9 terms in  $\psi_{mn}(\mathbf{c})$





#### Lattice Boltzmann Equation

• Equilibrium distribution function for  $f_{\alpha}$ 

$$
f_{\alpha}^{(eq)} = \rho w_{\alpha} [1 + \frac{3}{c^2} \boldsymbol{e}_{\alpha} \cdot \boldsymbol{u} + \frac{9}{2c^4} (\boldsymbol{e}_{\alpha} \cdot \boldsymbol{u})^2 - \frac{3}{2c^2} \boldsymbol{u} \cdot \boldsymbol{u}]
$$





Qian YH, d'Humieres D, Lallemand P. Lattice BGK Models for Navier Stokes Equation. Europhys Lett 1992;17:479-484.



## LBM MHD EP Model

**The model assumes coupling of the** velocity distribution function w/the Lorentz force **j** ×**B** in acceleration **a**  $\sim$   $\lambda$ 

$$
\frac{\partial f}{\partial t} + \mathbf{c} \bullet \nabla_{\mathbf{r}} f + \mathbf{a} \bullet \nabla_{\mathbf{c}} f = Q(f, f)
$$

**Then** 

$$
f(\mathbf{x} + \mathbf{c}\delta_t, \mathbf{c}, t + \delta_t) - f(\mathbf{x}, \mathbf{c}, t) = -\frac{1}{\tau} \Big[ f(\mathbf{x}, \mathbf{c}, t) - f^{(eq)}(\mathbf{x}, \mathbf{c}, t) \Big] - \frac{\delta_t}{2} \mathbf{a} \bullet \nabla_{\mathbf{c}} f
$$



## LBM MHD EP Model

- $\blacksquare$  Vector distrib.  $g(x, w, t)$  gives  $B = \int g dw$
- Macroscopic MHD eqs. also recovered
- **Evolution of**  $g(x, w, t)$  **obeys a kinetic equality**

$$
\frac{\partial \mathbf{g}}{\partial t} + \mathbf{w} \cdot \nabla \mathbf{g} = -\frac{1}{\lambda_m} \Big( \mathbf{g} - \mathbf{g}^{(eq)} \Big) = \frac{d \mathbf{g}}{dt}
$$
  
\n
$$
\mathbf{g}(\mathbf{x} + \mathbf{w}\delta_t, \mathbf{w}, t + \delta_t) - \mathbf{g}(\mathbf{x}, \mathbf{w}, t) = -\frac{1}{\tau_m} \Big[ \mathbf{g}(\mathbf{x}, \mathbf{w}, t) - \mathbf{g}^{(eq)}(\mathbf{x}, \mathbf{w}, t) \Big]
$$
  
\n
$$
\rho = \sum_{\alpha=1}^N f_\alpha \qquad \rho \mathbf{u} = \sum_{\alpha=1}^N \mathbf{e}_\alpha f_\alpha + (\mathbf{j} \times \mathbf{B}) \frac{\delta_t}{2} \qquad \mathbf{B} = \sum_{\beta=1}^M \mathbf{g}_\beta
$$

Dellar, P., "Lattice Kinetic Schemes for MHD", Journal of Computational Physics **179,** 95–126 (2002). G. Breyiannis and D. Valougeorgis, "Lattice kinetic simulations in three-dimensional magnetohydrodynamics", PHYS. REV. E **69**, 065702(R) (2004)



## LBM MHD Parameters

- **The magnetic resistivity** is  $\eta = \tau_m \theta_m \delta_t$
- where  $\theta_m = 1/4$
- Constraints are

$$
\Sigma_{\beta} W_{\beta} = 1, \Sigma_{\beta} W_{\beta} \zeta_{j\beta} \zeta_{\beta j} = 0
$$

- **For lattice to retain** symmetry up to 3<sup>rd</sup> order:
- $\Sigma_{\beta}$  *W<sub>β</sub>* $\zeta_{\beta\alpha}$ =0,  $\Sigma_{\beta}$  *W<sub>β</sub>* $\zeta_{\beta\alpha}$  $\zeta_{\beta j}$  $\zeta_{\beta\gamma}$ =0



$$
g_{\beta j}^{(eq)} = W_{\beta} \left[ B_j + \theta_m^{-1} \zeta_{\beta i} \left( u_i B_j - B_i u_j \right) \right]
$$
  

$$
W = \begin{bmatrix} 1/4, & \beta = 0 \end{bmatrix}
$$

 $W_{\beta} =$  $1/2, \quad \beta = 1, 2,...6$  $\left\{ \right.$  $\lfloor$ 



#### Electron/Ion number density mappings

- **NASA Solar Electric** Propulsion Technology Applications Readiness (NSTAR) 30-cm ion thruster
- **Thruster operating** conditions:  $V_{dc} = 25.10$  V and  $J_{dc} = 8.24 \text{ A}$
- **LBMHD #density nozzle** expansion characteristics partly captured
- But not range of #s

malized Axial Position 2 ni [cm 3]  $1E + 13$  $1.5$  $5E+12$  $1E + 12$  $5E+11$  $1E + 11$  $0.5$ 5E+10  $1F + 10$ 5 Normalized Radial Position from Centerline **DCA** 



Daniel A. Herman† and Alec D. Gallimore, "Discharge Chamber Plasma Structure of a 30-cm NSTAR-type Ion Engine" Plasmadynamics and Electric Propulsion Laboratory, U. Michigan, Ann Arbor, MI 48109 USA, AIAA-2004-3794



# Velocity map

- Xe II velocity map for 12 A, 27 V operation.
- **Note regions of back-flowing** ions along the cathode face (x=0) & region of small velocities along centerline between 0.3 & 0.6 cm downstream.
- Some individual species effects on plasma stream at centerline & edges
- **LBMHD captures major plasma** flow, not back-flow details



G. J. Williams, Jr., T. B. Smith, K. H. Glick, Y. Hidaka, and A. D. Gallimore, "FMT-2 Discharge Cathode Erosion Rate Measurements via Laser-Induced Fluorescence", AIAA-00-3663



# Velocity map

- Xe II velocity map for 12 A, 27 V operation.
- **Note regions of back-flowing** ions along the cathode face (x=0) & region of small velocities along centerline between 0.3 & 0.6 cm downstream.
- **LBMHD w/a little more plasma** turbulence captures more of the flow trends and some back-flow



G. J. Williams, Jr., T. B. Smith, K. H. Glick, Y. Hidaka, and A. D. Gallimore, "FMT-2 Discharge Cathode Erosion Rate Measurements via Laser-Induced Fluorescence", AIAA-00-3663



## Conclusions & Future Work

- **LBMHD does OK modeling EP bulk fluid flow**
- **Other species back-flow too buried in MHD** plasma model
- **Electrostatic single species model does better** as in **LBM-Poisson model of optics**\*
- **Next is to try** 
	- other species, perhaps quasi-3D w/Maxwell's eqs.
	- variations in collision operator, e.g.,pseudo-random collision frequency as in DSMC
	- Other variations of BE form

<sup>\*</sup> Richard, J. C. and Shah, P. Application of LBM to Xe<sup>+</sup> Flow about Ion Thruster Optics", Int'l. Conf. for Mesoscopic Methods in Engineering and Science (ICMMES), Technical University of Braunschweig, Germany, July 26 - 29, 2004 www.icmmes.org

